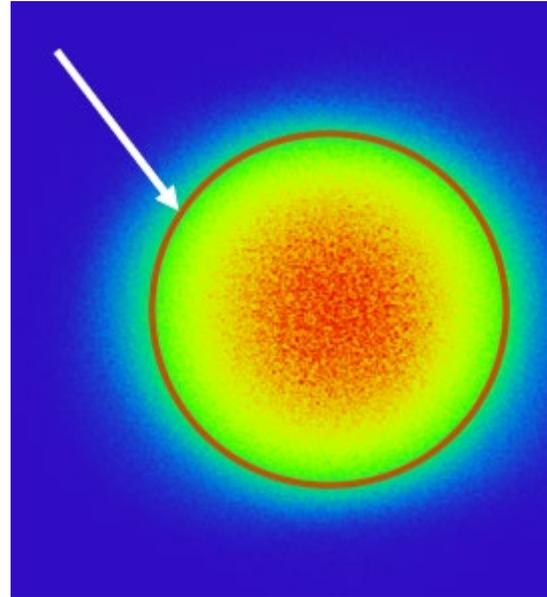


# Design and Performance of a Heliostat with a Twisting Mechanism to Maintain Focus Through the Day

Presentation for SolarPACES  
2023

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Sciences

# Why focusing heliostats?

- Goal: Store energy at higher temperatures
  - Higher Carnot efficiency
  - Solar industrial process heat (SIPH)
- Need higher concentration at receiver
- Current CSP recipe:
  - Flat heliostats, small compared to receiver
  - Contribution from each one is small
  - Takes  $\sim 50,000$  heliostats to get 500x concentration on the receiver

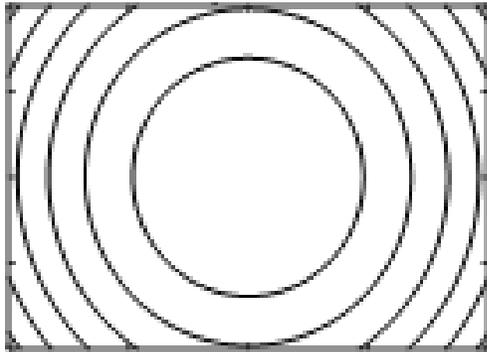


- Focusing heliostats concentrate sunlight 10-30x depending on focal length
  - Can achieve high concentration/temperature with far fewer
- Can focusing be made simply such that the added cost is low enough to make economic sense?

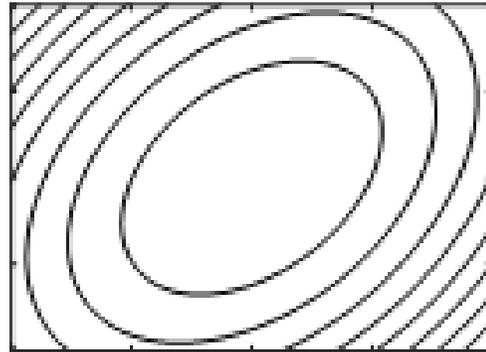
# Maintaining focus throughout the day

- A fixed concave shape loses focus as the sun moves
- Active shape changing is needed to maintain a focus throughout the course of a day
- Contours below from ray-trace modeling show the different biconic reflector shapes needed from early morning to late afternoon for a representative heliostat

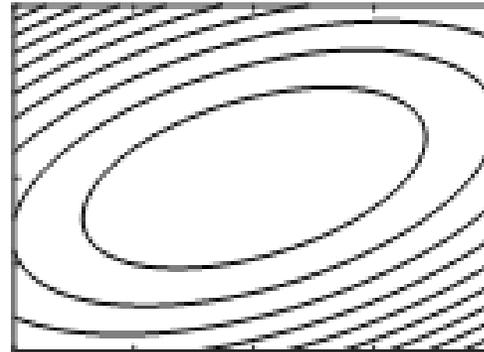
7:30 AM - 4° AOI



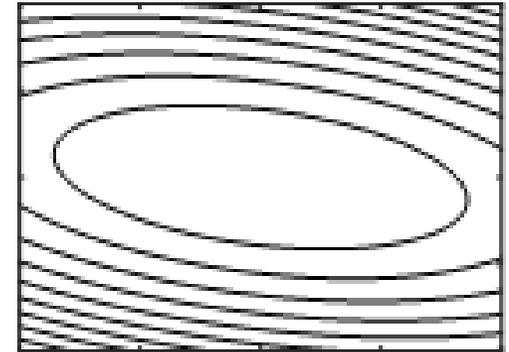
2:30 PM - 50° AOI



4:30 PM - 65° AOI



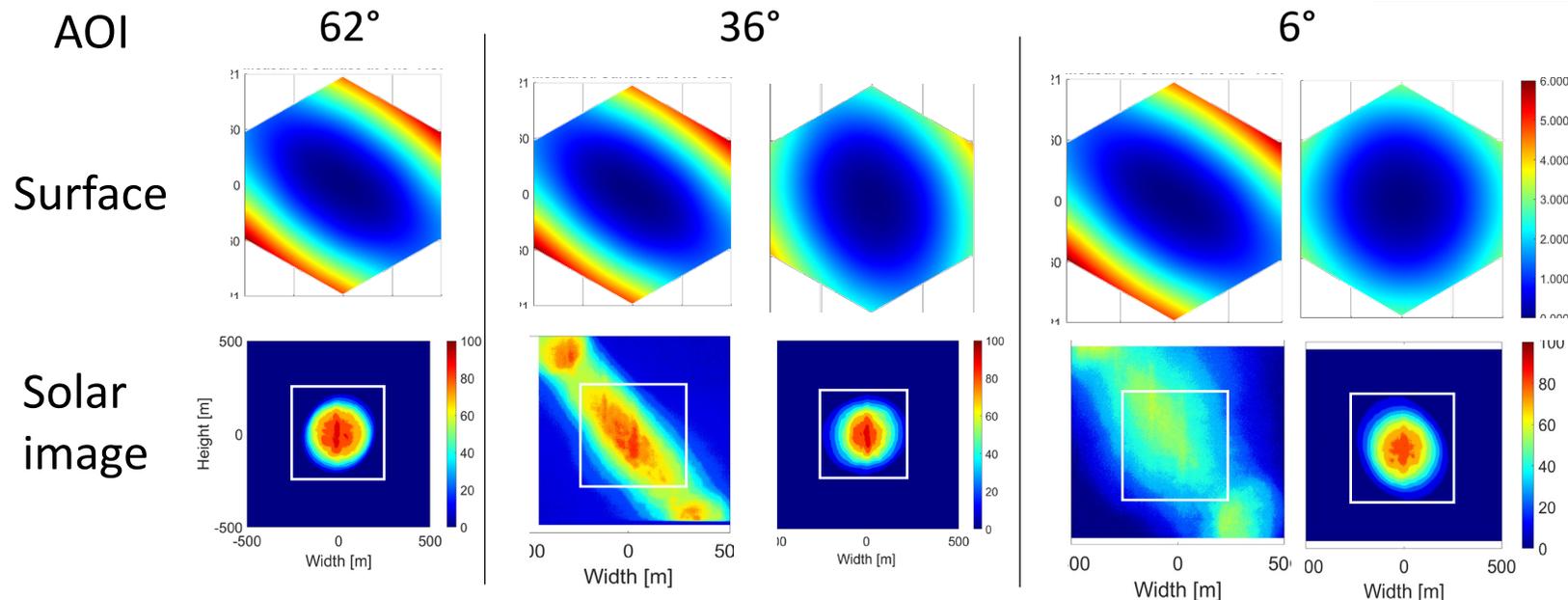
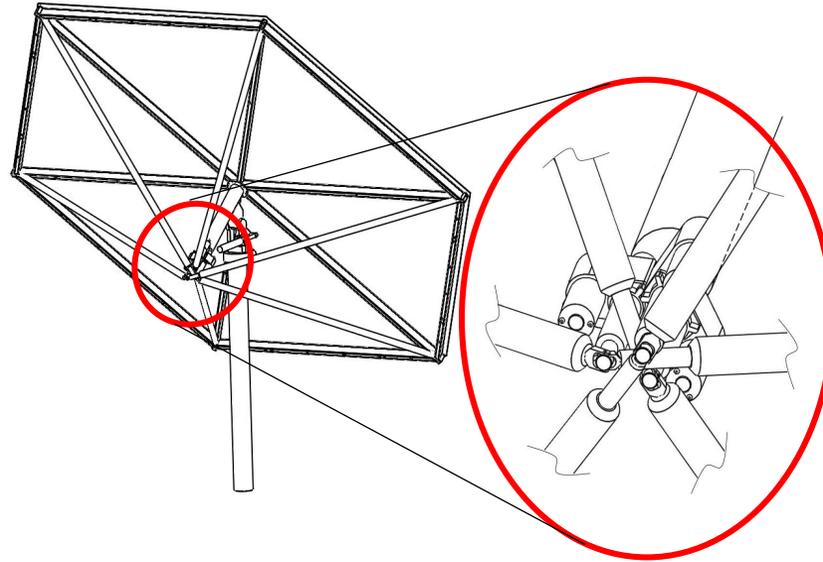
5:30 PM - 72° AOI



- For heliostat due W of a receiver at 20° elevation, equinox, 33° lat.
- Ellipse axis rotates through the day

# 2020 field test with hexagonal heliostat

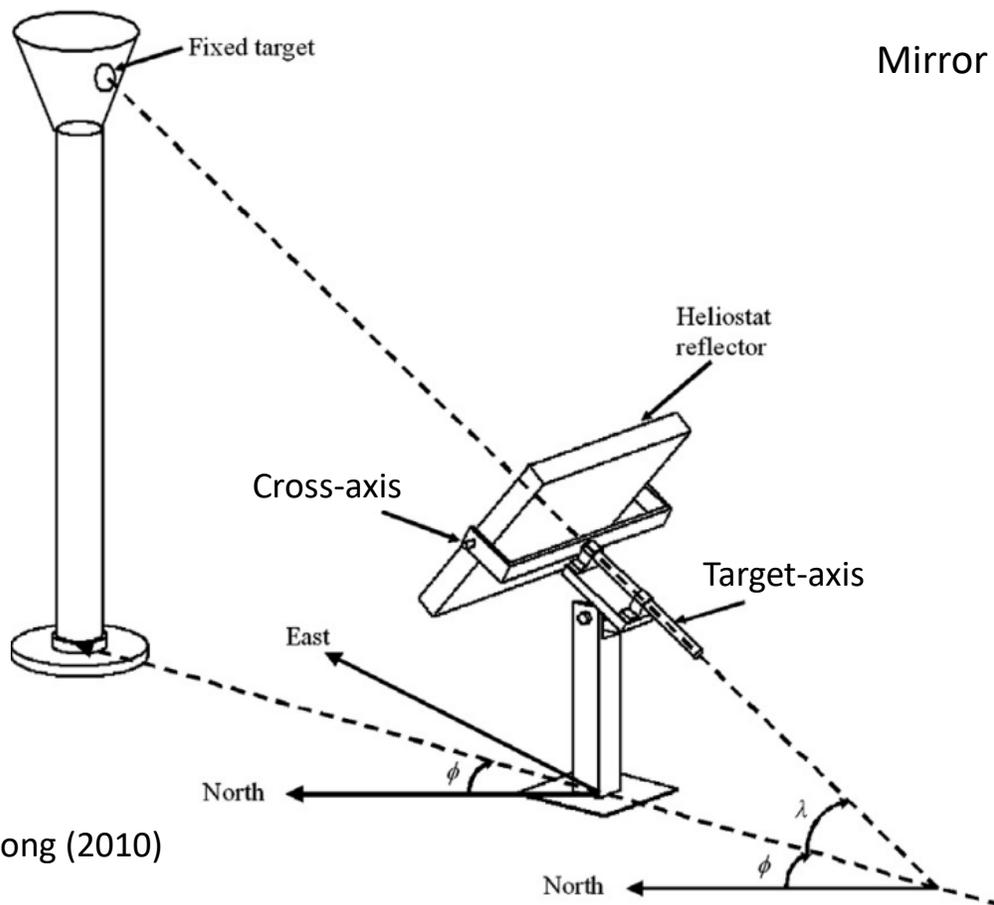
- Attach reflector panel to frame, set initial shape with support pads
- Connect back struts from corners to central nodes
- 3 computer- controlled actuators to set shape



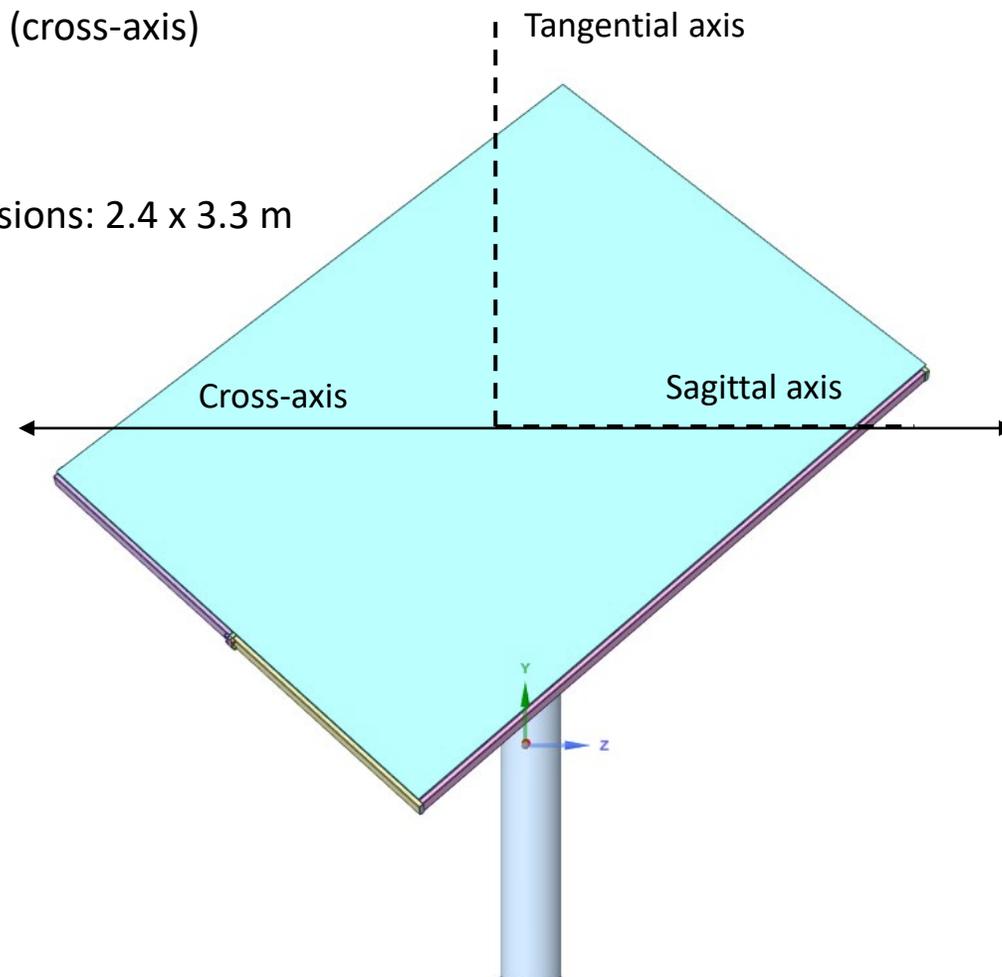
Solar disc image obtained at 2:30 pm, screen 40 m to the East, 62° AOI

# New approach – Target-axis mount

- One axis points to receiver (target-axis), the other runs perpendicular (cross-axis)
- Target axis and solar vector form the plane of incidence
- Mirror is rotated 45 degrees relative to cross-axis

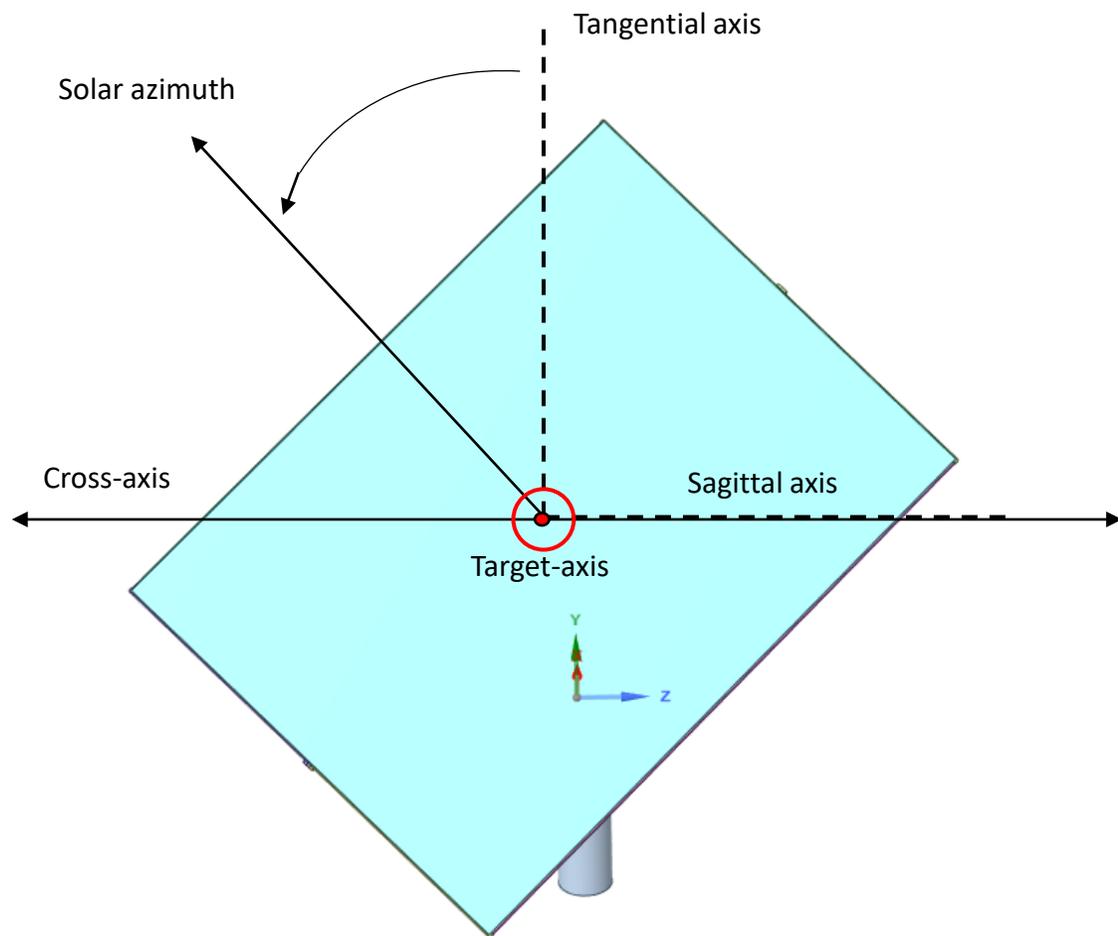


Mirror dimensions: 2.4 x 3.3 m

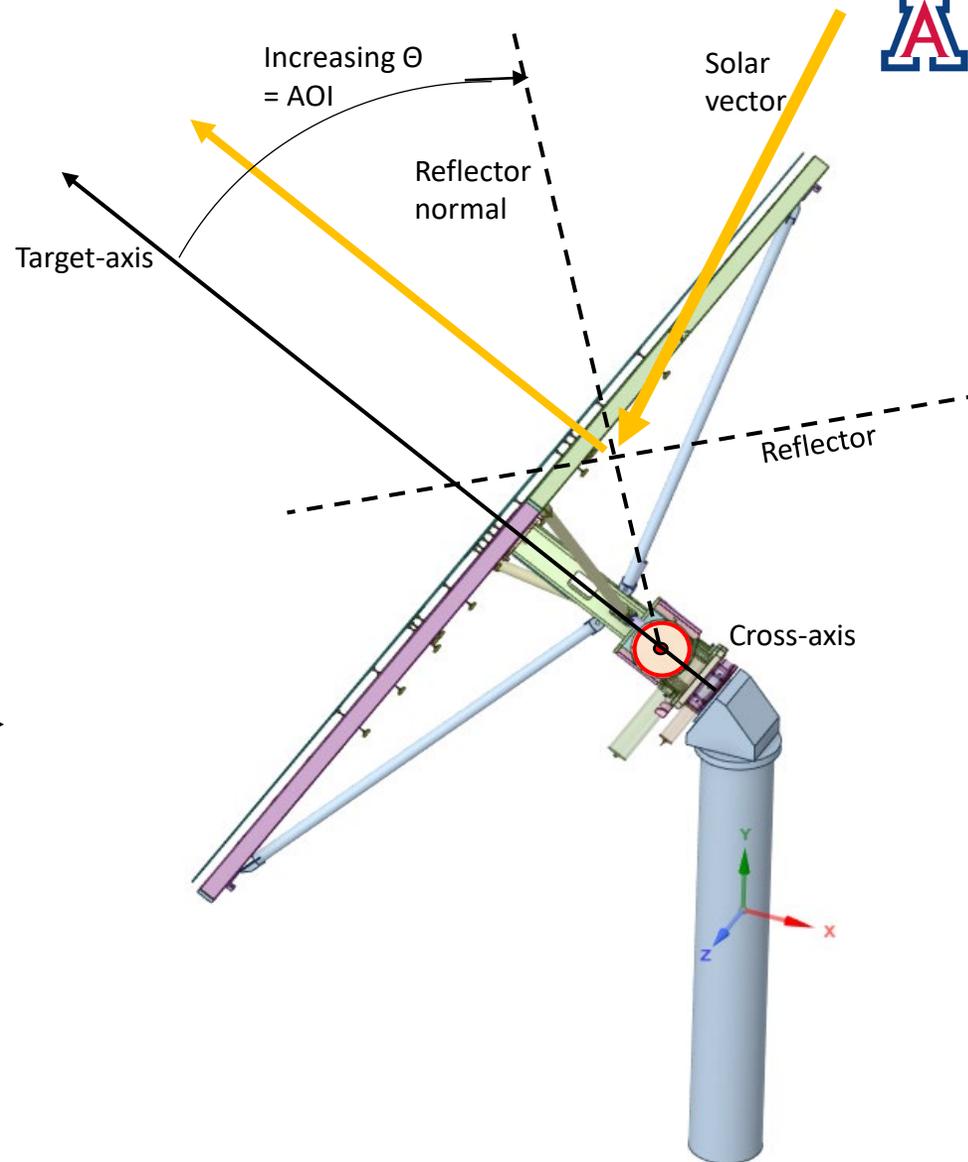


K. K. Chong (2010)

# Pointing

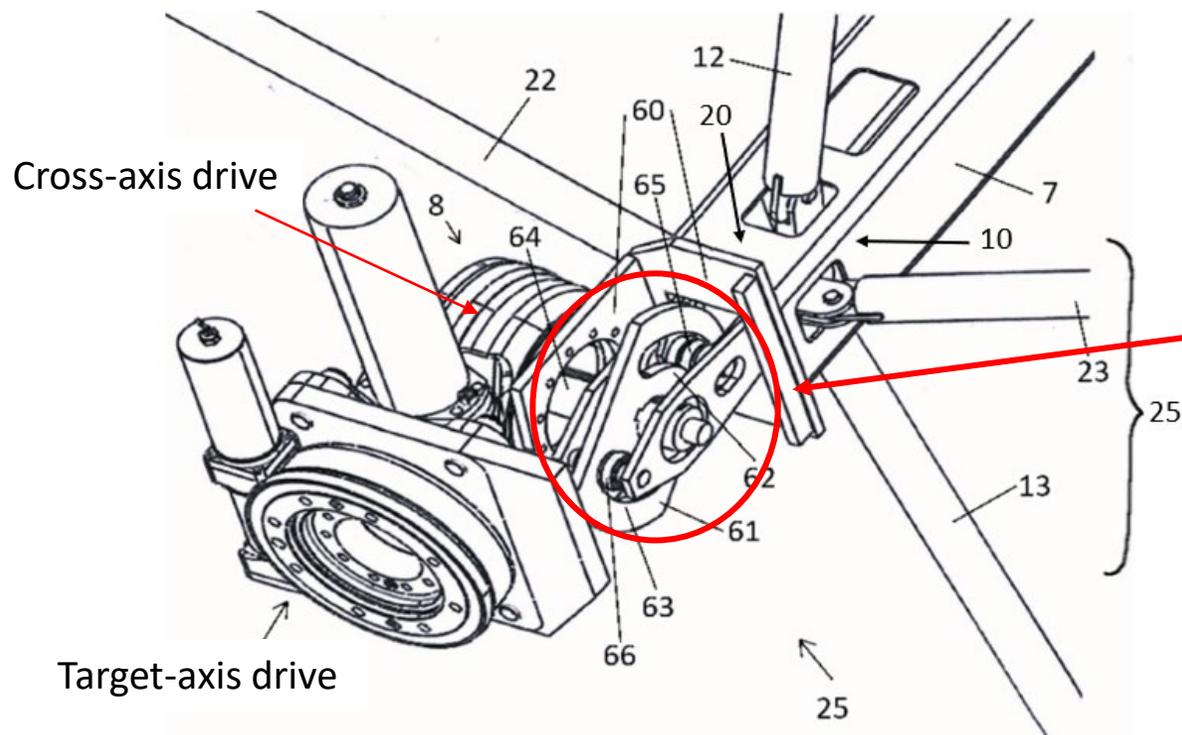


Tangential axis is aligned to plane of incidence

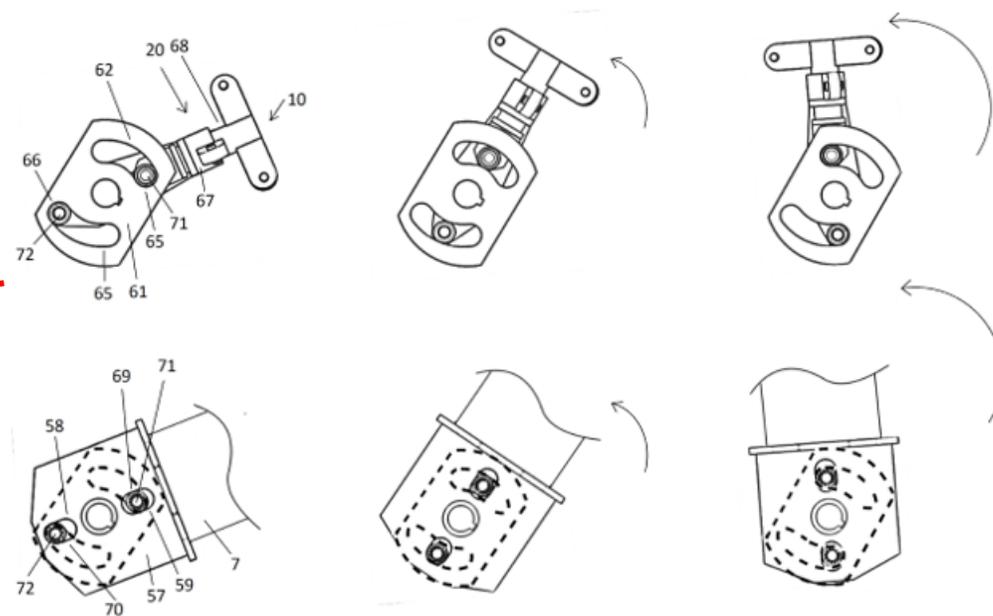


Cross-axis angle = angle of incidence

# Passive shape changing – no actuators required



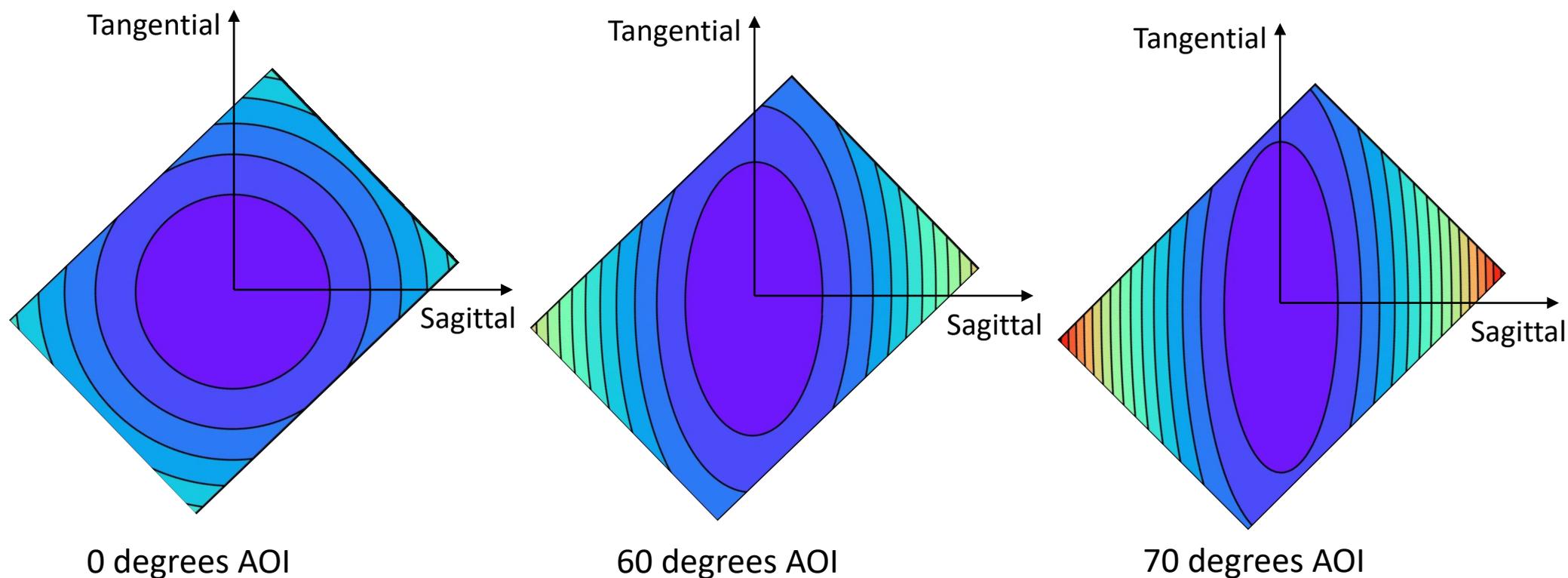
Cam and wheel linkage between cross-axis drive and back struts



Interface plates

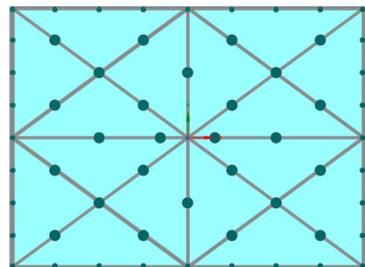
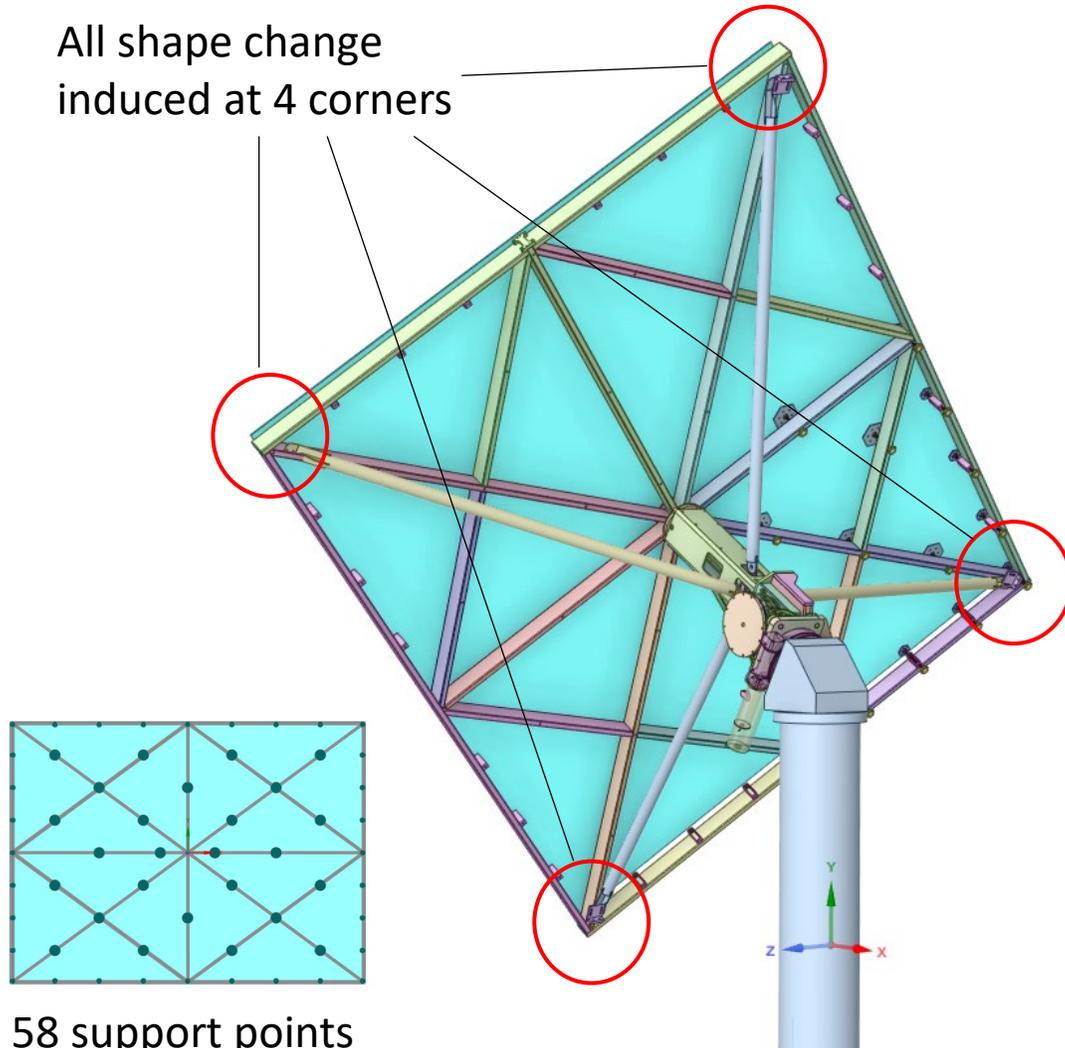
# Ideal biconic shapes for 113 m focal length

- Biconics are in a fixed orientation on the mirror for target-oriented mount



# “Twisting” heliostat

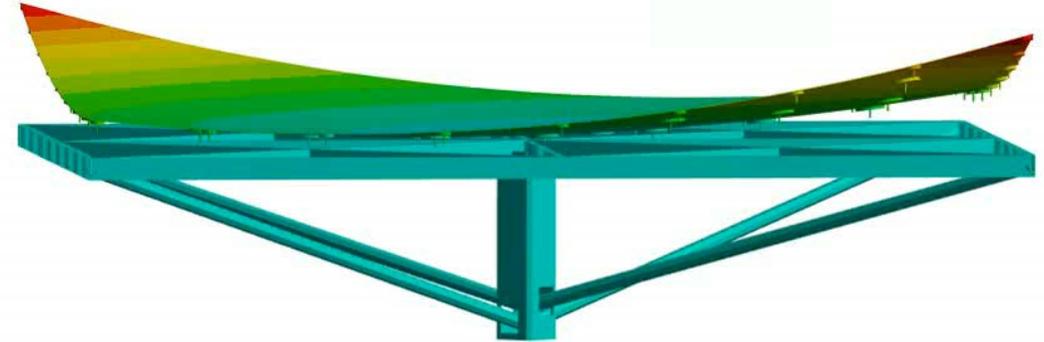
All shape change induced at 4 corners



58 support points

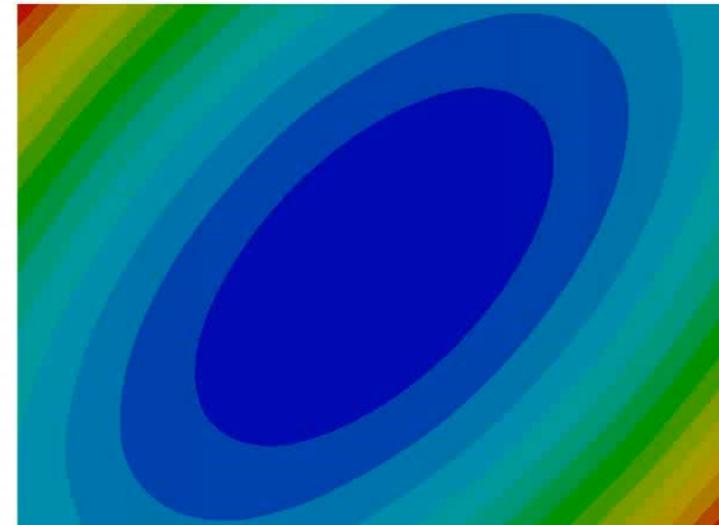
0: 0 degrees AOI outer  
 Directional Deformation 2  
 Type: Directional Deformation(Z Axis)  
 Unit: in  
 Global Coordinate System  
 Time: 2 s  
 10/7/2023 1:15 AM

0.62517 Max  
 0.55868  
 0.4922  
 0.42572  
 0.35924  
 0.29276  
 0.22628  
 0.1598  
 0.093314  
 0.026832  
 -0.039649  
 -0.10613  
 -0.17261  
 -0.23909  
 -0.30558 Min



0: 0 degrees AOI outer  
 Directional Deformation  
 Type: Directional Deformation(Z Axis)  
 Unit: in  
 Global Coordinate System  
 Time: 2 s  
 10/7/2023 1:18 AM

0.62517 Max  
 0.58349  
 0.54181  
 0.50013  
 0.45846  
 0.41678  
 0.3751  
 0.33342  
 0.29175  
 0.25007  
 0.20839  
 0.16671  
 0.12503  
 0.083357  
 0.041679  
 1.8239e-6 Min

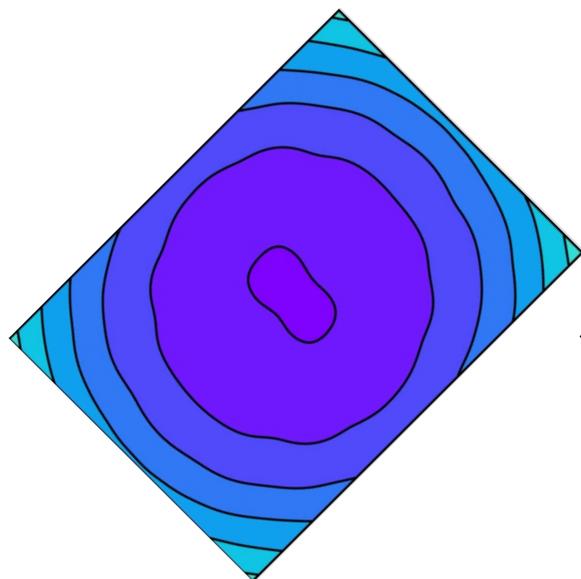


Shape change from 60 to 0 degrees AOI

# Modeled performance

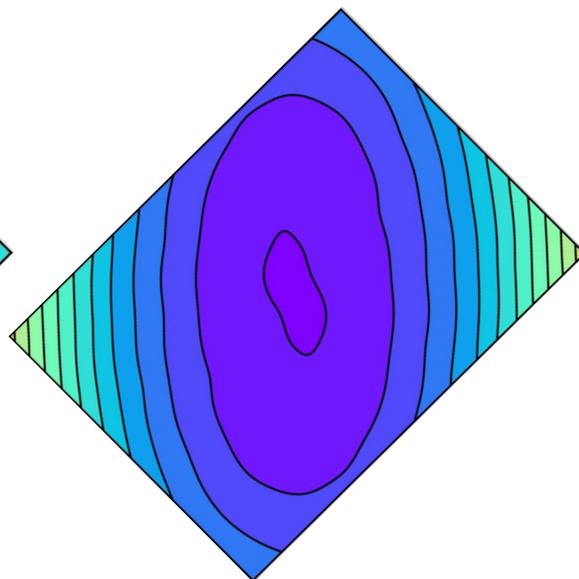
- Twisting, gravity + 11 mph headwind at 30-degree impingement (Peterka 1992, GEC 2003)
- RMS slope error < 0.7 mrad
- Encircled energy in 1 m diameter: 89%

RMS: 0.66 mrad



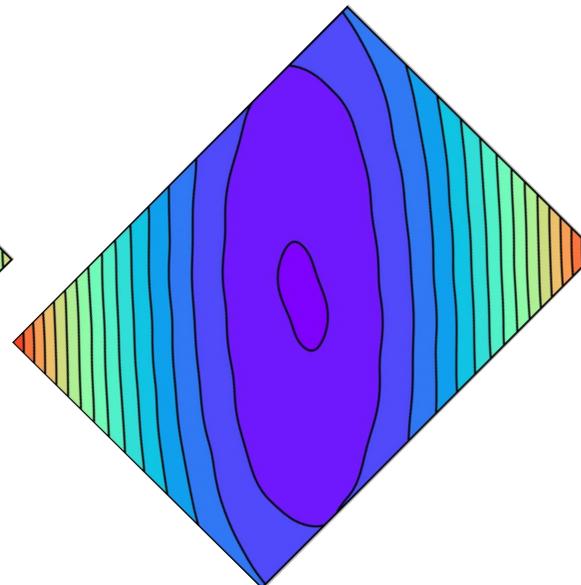
0 deg AOI

RMS: 0.53 mrad



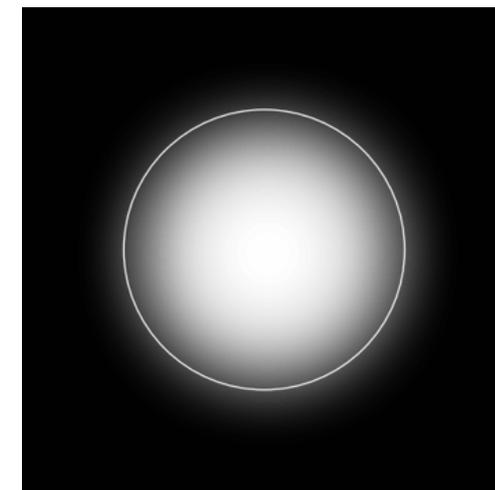
60 deg AOI

RMS: 0.63 mrad



70 deg AOI

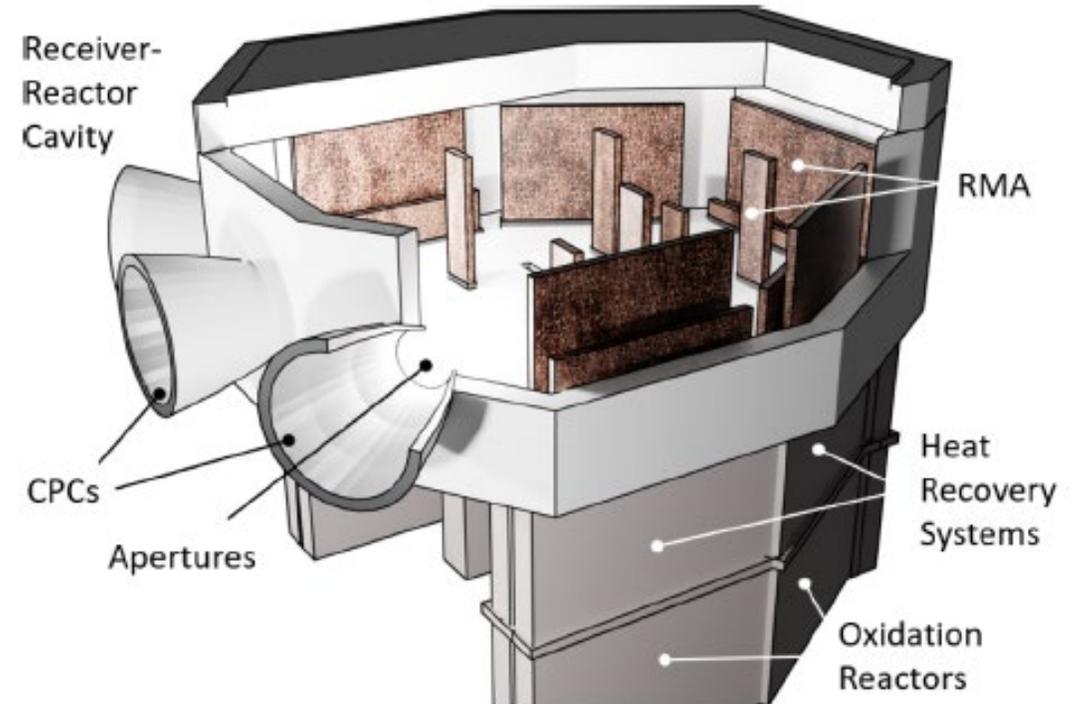
Encircled Energy: 89%



Energy in 1 m diameter circle

# Applications

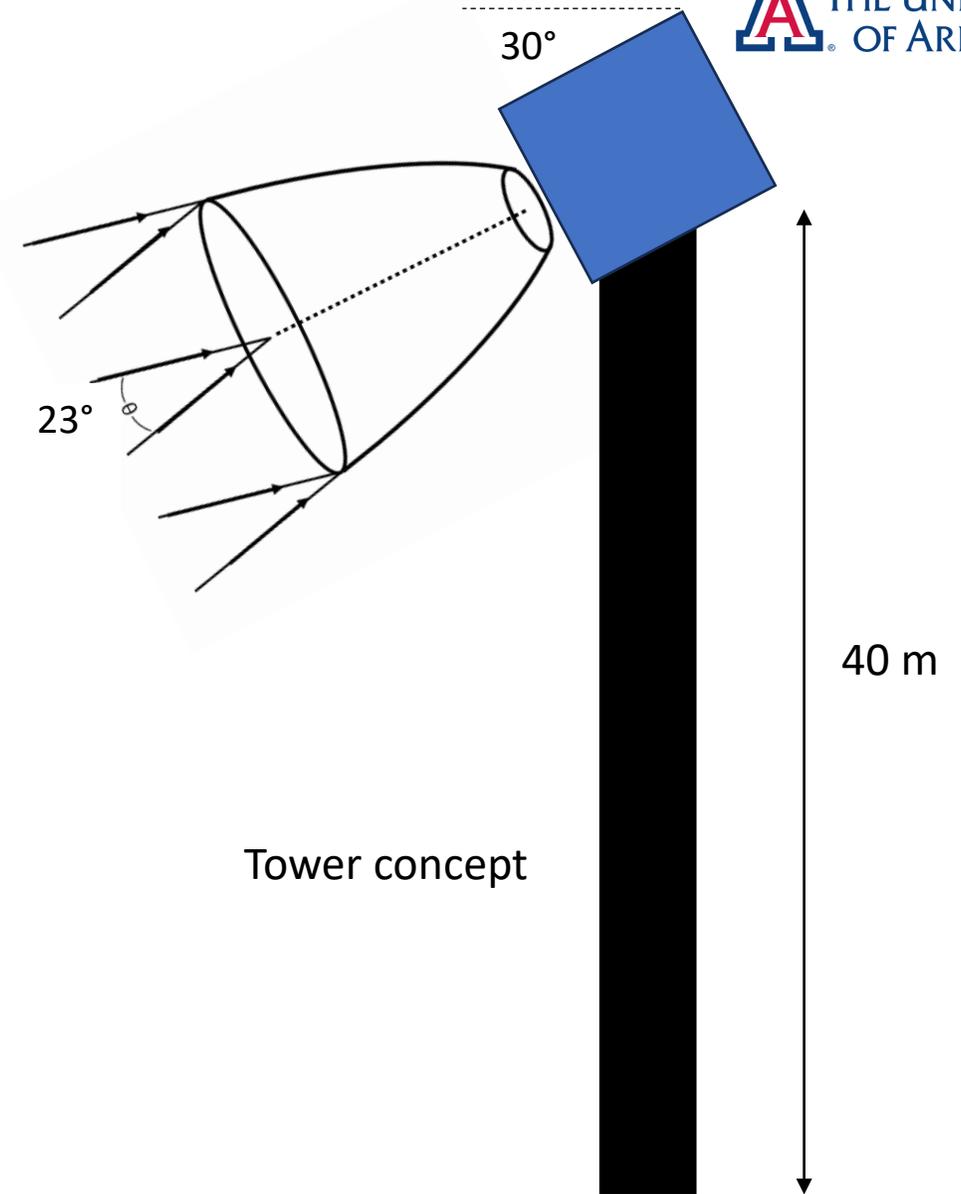
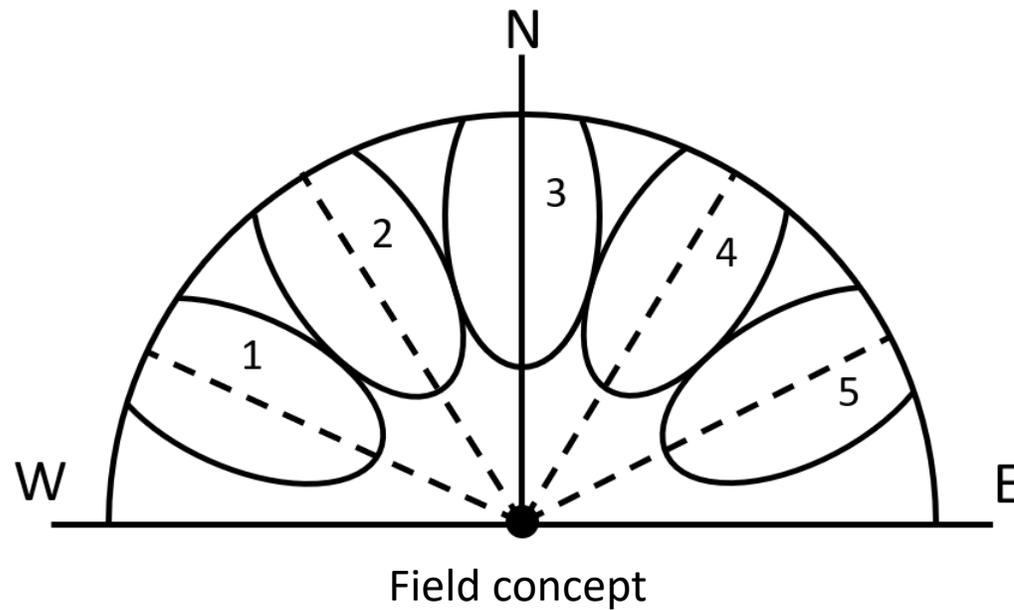
- Traditional surround field
  - 2000 twisting heliostats, 1.2 x 1.2 m receiver, 1700x concentration, 11 MW (R. Angel 2022)
- Solar industrial process heat (SIPH) requiring  $T > 1000^{\circ}\text{C}$
- Examples: Making cement from lime and thermochemical water splitting
- Temperatures of  $\sim 1500\text{ C}$  require concentrations  $\sim 3000\text{x}$
- Can be reached through the day by a field of twisting heliostats feeding CPCs (Compound parabolic concentrators)



Brendelberger et al. (2022)

# CPC tower/field concept

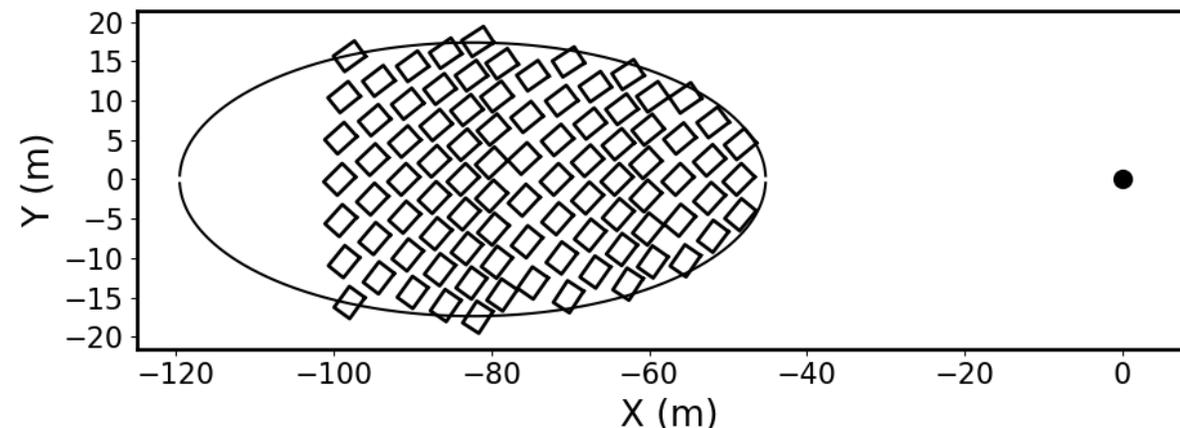
- CPC entrance pupil: 1 m
- CPC concentration: 10x
- 5 CPCs accepting light from 5 groups of heliostats



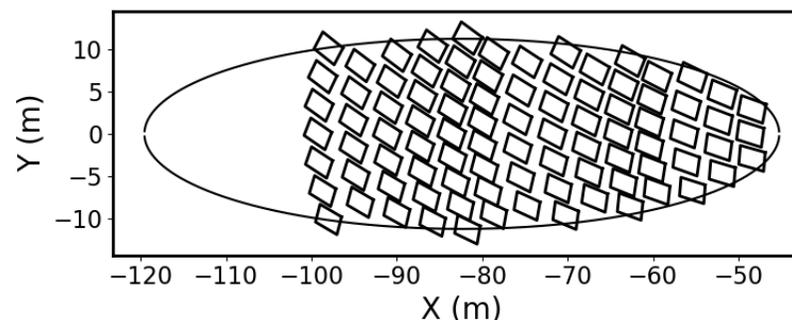
# Heliostat layout and field throughput

- 90 heliostats
- Total ground area: 1600 m<sup>2</sup>
- Total heliostat area: 720 m<sup>2</sup>
- Spaced 45 – 100 m from tower
- Focal lengths: 70 – 110 m
- Avg cosine factor: 0.8
- Avg shadowing/blocking: 9%
- **Geometric throughput: 73%**

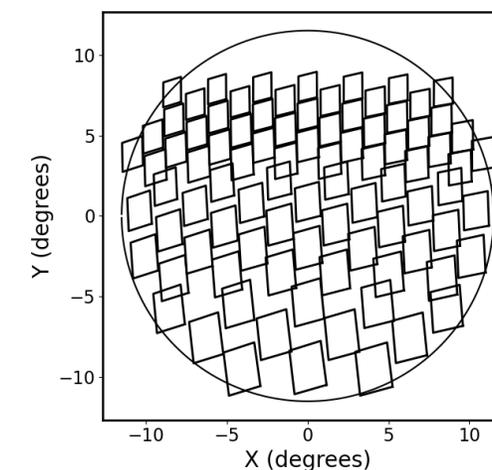
Field plan view



Sun view



Receiver view



# Total optical throughput and concentration

Throughput source	Fraction
Spillage	0.89
Geometric throughput	0.73
Heliostat reflectivity	0.9
CPC reflectivity	0.9
CPC window transmission	0.9
<b>Solar concentration calculation</b>	
Total throughput (fraction of heliostat area)	0.47
Total heliostat area	720 m <sup>2</sup>
Effective area of sunlight	341 m <sup>2</sup>
CPC entrance pupil area	0.79 m <sup>2</sup>
CPC concentration	10x
<b>Total solar concentration</b>	<b>4316x</b>

# Design/analysis summary

- Individual twisting heliostat
  - Shape changing is passive – no actuators required
  - Finite element analysis shows an individual heliostat can be shaped to  $<0.7$  mrad RMS slope accuracy in the field
- Field design with CPCs
  - 450 heliostats,  $3600 \text{ m}^2$  total mirror area
  - 1.6 MW into receiver
  - Twisting heliostat field and CPC can deliver solar concentrations  $> 4000x$  with CPC

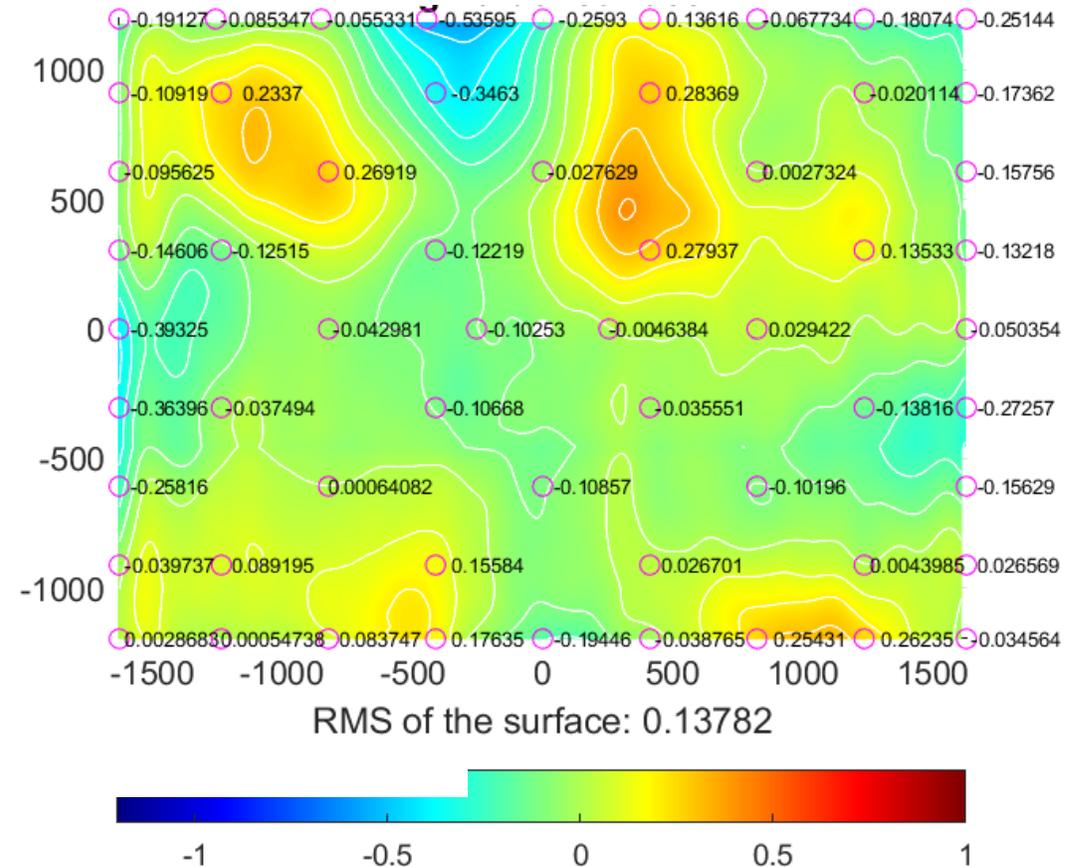
# Prototype construction and metrology

- current status



# Measured surface shape of 3.3 x 2.4 m reflector

- Surface set by adjusting 58 points for
  - 113 m focal length
  - Biconic needed for 60° AOI
- Contour map, measured by reflectometry with 1 in. spatial resolution, shows departure from ideal biconic shape
- Surface error is 140  $\mu\text{m}$  rms
- Same surface error when twisted to 0° AOI

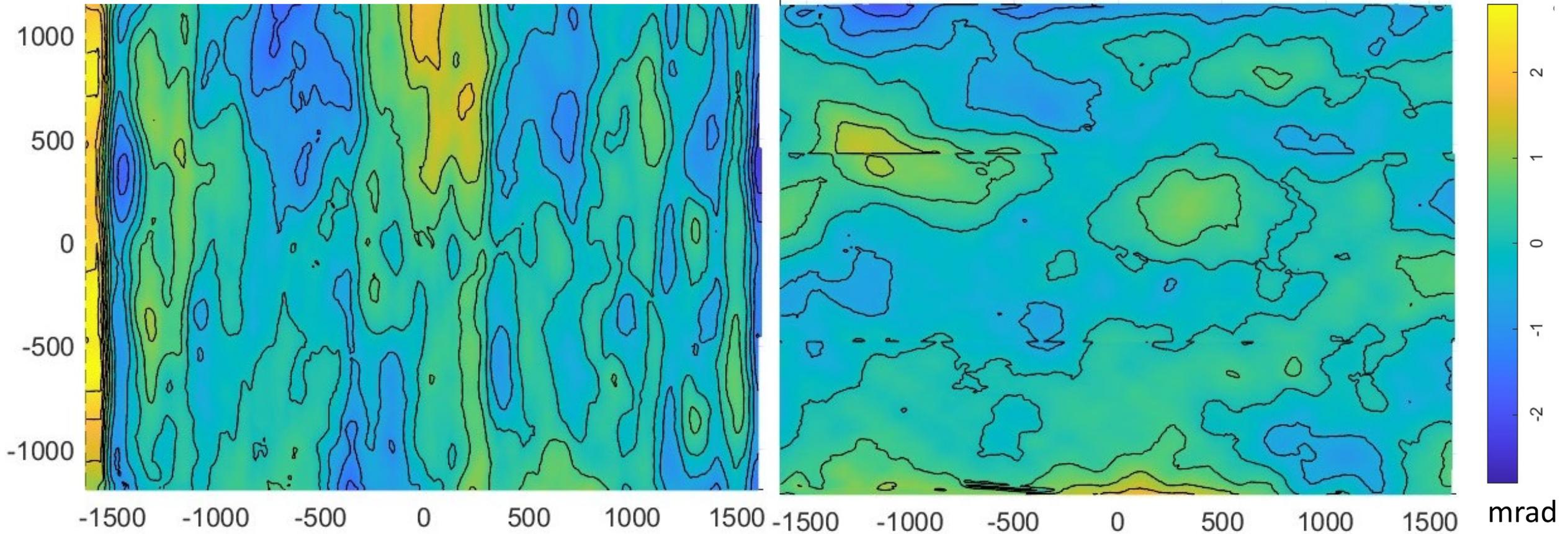


# Slope errors of the same reflector

– departure from fitted biconic surface

y slope accuracy limited by adjustment accuracy to 0.41 mrad rms

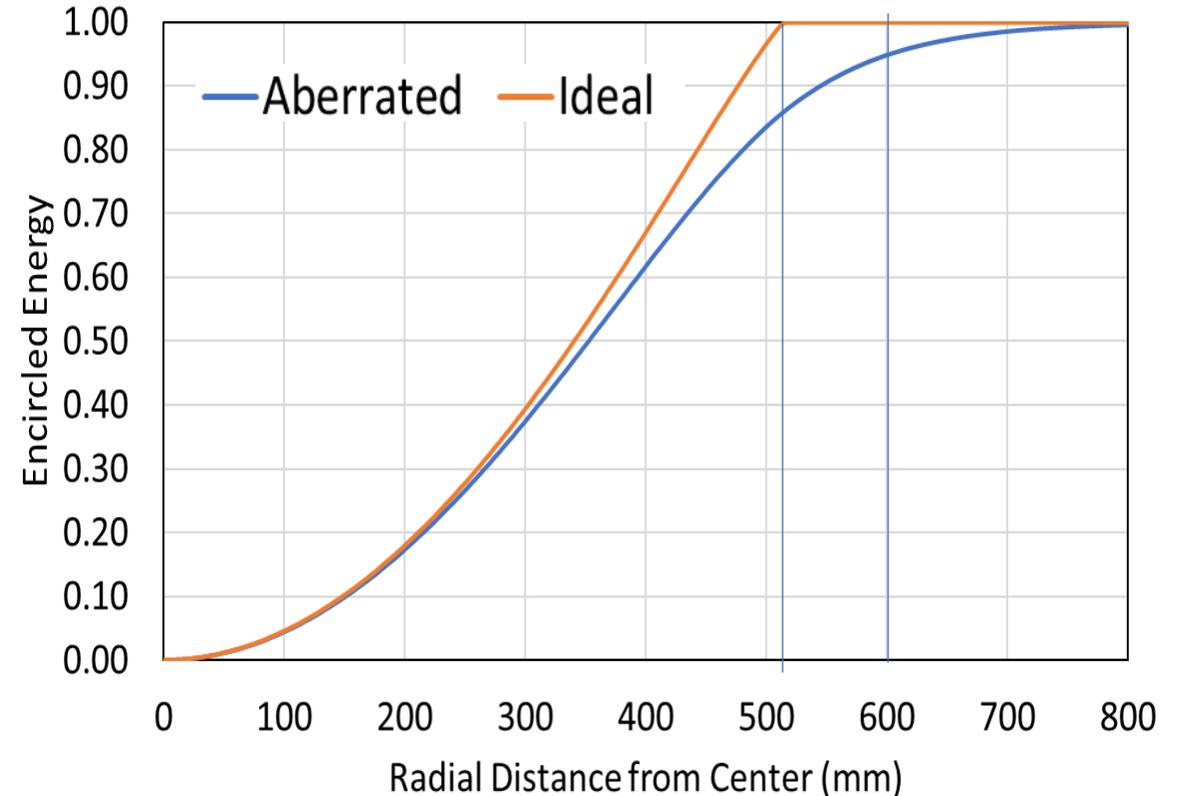
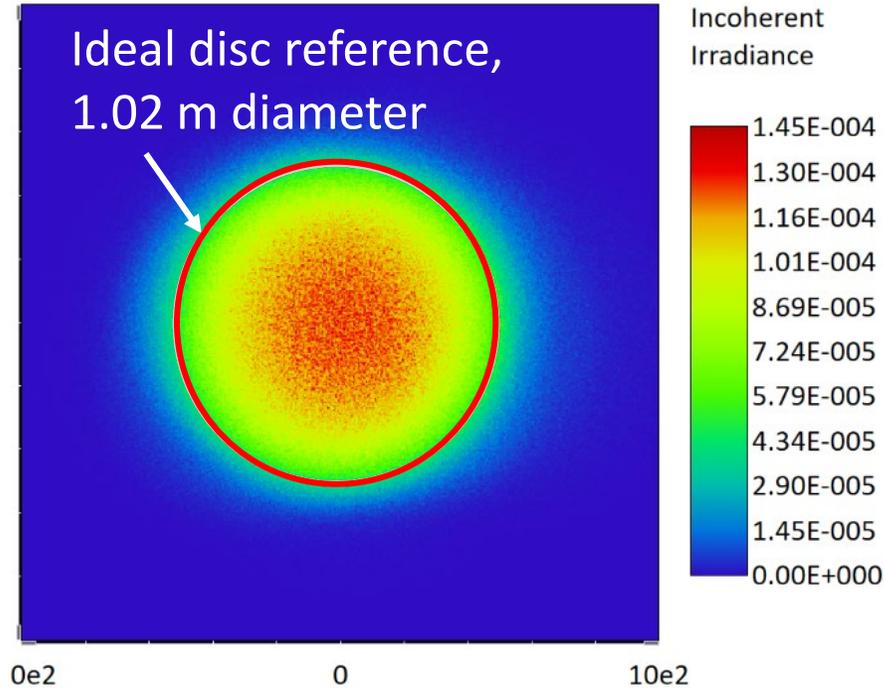
x slope shows added vertical ripples of 0.52 mrad rms from float glass manufacture



x slope 0.66 mrad rms

y slope 0.41 mrad rms

# Disc image calculated for measured surface

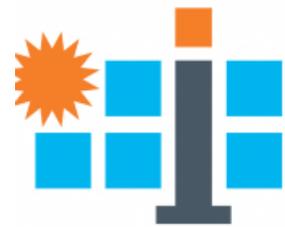


- Image at 113 m focal distance

- Encircled energy
  - 86% in ideal 1.02 m dia.
  - 95% in 1.2 m diameter

# Next steps/Acknowledgements

- Next steps
  - Complete tracker assembly, and mechanical coupling mechanism
  - On sun testing at University of Arizona Tech Park
  - Test prototype at Sandia National Labs NSTTF with Co-I Randy Brost
- US Department of Energy
  - Small Innovative Projects in Solar (SIPS)
  - HelioCon



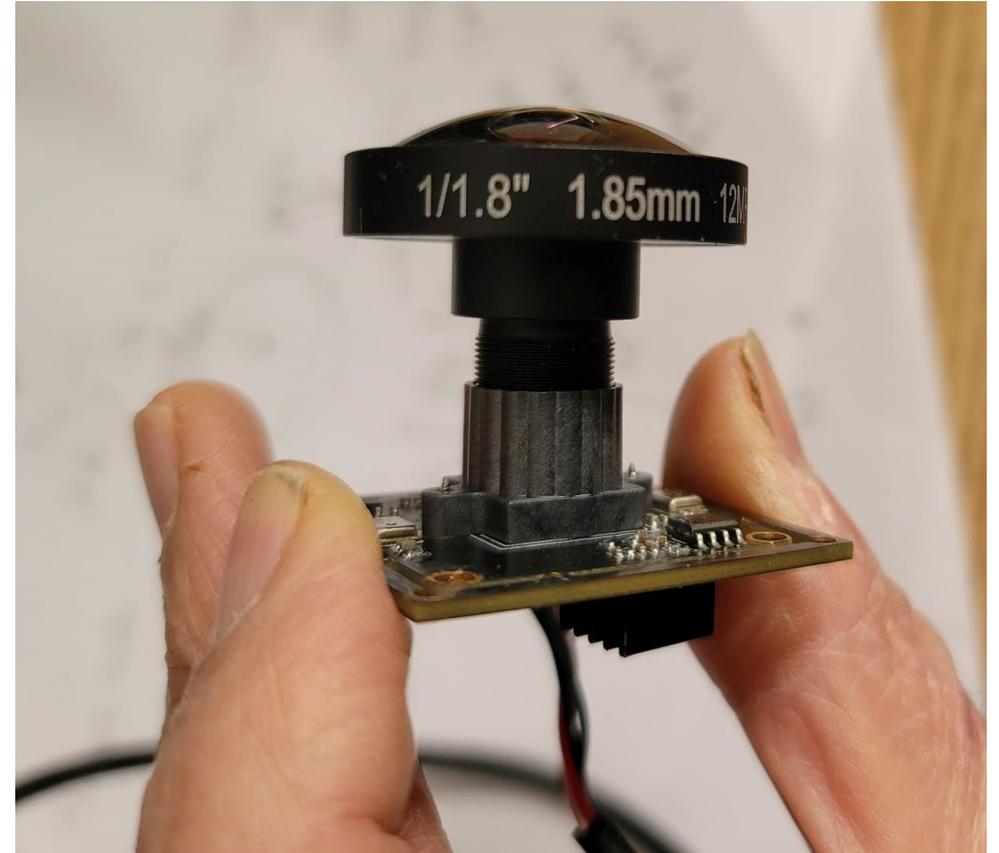
U.S. Department of Energy

# HelioCon

HelioCon Consortium for  
Concentrating Solar-Thermal Power

# Closed-loop tracking

- Wide angle camera mounted behind glass with center section of silvering removed
- Camera to be rigidly attached in fixed position relative to mirror normal and tangential axis
- Views simultaneously the sun and a distant LED source at fixed location
- Control loop uses observed positions of the LED source and sun



# Fatigue life analysis

- Based on published Weibull statistics for float glass (Pisano 2015) and subcritical crack growth mechanics
- Annual wind speed distribution from Lee Ranch, NM, USA (GEC 2003)
- Wind loads calculated by Peterka 1992
- Computed mirrors stresses vs wind speed for worst case load configuration
  - 30-degree impingement up to 50 mph, stow position up to 90 mph
  - Inner row heliostat at 70-degree AOI bending

Survival probability ~ 90% after 30 years

